

1 A method for estimating daily loads from coastal watersheds with adjustments for dilution and
2 concentrating effects, utilizing the National Hydrography Dataset Plus Estimated Runoff Model. By
3 Karen R. Worcester and David M. Paradies. Central Coast Ambient Monitoring Program. 2015 draft.
4

5 **Abstract**

6 We describe an approach for estimating daily flows and loads from small coastal streams in
7 central coastal California. Estimations are derived from monthly measured flow and concentration data,
8 coupled with daily flow and dilution models. Daily flow estimation makes use of average annual stream
9 flow estimates from the National Hydrography Dataset Plus Estimated Runoff Model (EROM). From
10 locally available stream gage data, daily ratios are developed between daily flow averages and the EROM
11 average annual flow estimates for each gage location. Where multiple gages are used, the ratios are
12 averaged. These ratios are then applied to the EROM average annual stream flow estimates at nearby
13 stream sampling locations to estimate daily flows. Measured monthly flows are used as benchmarks to
14 assess performance.

15 Loading estimates derived from linear interpolation of monthly flow and concentration data are
16 likely to have a high degree of error because of intervening storm events which may dramatically effect
17 loading and may cause dilution effects. In some cases high flow may reduce concentrations due to
18 dilution and in other cases, pollutants may increase in concentration with flow because of overland
19 transport. We characterize this relationship at the scale of individual watersheds and describe a method
20 for improving the accuracy of loading estimates by application of watershed specific relationships
21 between pollutant concentration and flow.
22

23 **Introduction**

24 The California central coast is characterized by relatively small coastal watersheds that in some
25 cases transport relatively high loads of pollutants to the Pacific Ocean. Few of these watersheds contain
26 flow gages and very few contain any water quality instrumentation, but monthly water quality and flow

27 data is available from the Central Coast Ambient Monitoring Program (CCAMP) and related efforts. An
28 approach was needed to better characterize flows and loads leaving these watersheds; there is a
29 continuing need to understand pollutant loading to the ocean in support of epidemiological studies of
30 marine mammal disease (M.A. Miller et al., 2002; M.A. Miller et al., 2005; W.A. Miller et al., 2006;
31 Stoddard et al, 2008), studies on the role of anthropogenic nutrient inputs in plankton bloom initiation
32 (Lane et al., 2009, Kudela et al., 2008; Ryan, et al., 2008), and other purposes. Our approach is adaptable
33 to other areas where local gage data and stream flow and water quality measurements are available.

34 CCAMP is the California Central Coast Water Board's regionally-scaled water quality
35 monitoring program. It operates along a 300-mile stretch of California coastline from southern San
36 Mateo County through northern Ventura County. CCAMP's "Coastal Confluences" monitoring program
37 provides a long-term dataset of monthly stream flow and water quality measurements at the ocean
38 discharge point of thirty-three streams and rivers. Associated watersheds range in size from X to Y
39 square kilometers.

40 The Central Coast Daily Flow Estimation (CCDFE) approach described here utilizes annual
41 average flow estimates available within the National Hydrography Dataset Plus Version 2 (NHDPlus V2)
42 (Horizon Systems, 2005) and improves upon these estimates for more locally-scaled purposes, using
43 locally available stream gage and flow measurement data. NHDPlus V2 is a suite of nationally scaled
44 geo-spatial datasets that provide a hydrologic framework for analysis, and that integrate features from the
45 the National Hydrography Dataset, National Elevation Dataset, and the Watershed Boundary Dataset
46 (McKay, L. et al., 2012).

47 Included in the NHDPlus V2 geospatial framework is the Estimated Runoff Model (EROM),
48 which estimates average annual flows for each NHD stream catchment. Runoff is derived from a "flow
49 balance model" (Wolock and McCabe, 1999), which incorporates precipitation, potential
50 evapotranspiration, evapotranspiration, and soil moisture storage (McCay, et al., 2012). Incremental
51 flows are calculated by routing and accumulating catchment level flows using NHDPlus flow lines. This
52 estimate of "natural" runoff is further refined when necessary by accounting for instream losses due to

53 natural hydrologic processes, an important correction for flow estimates in the arid West. The estimate is
54 also corrected for a negative bias in base flow estimates through a log-log regression-based adjustment
55 using “reference” gage data from largely unaltered river and stream systems (McCay, et al., 2012). The
56 model can account for flow additions, removals and transfers where data is available. Flow estimates are
57 adjusted where on-stream flow gage data is available, pro-rating for differences in drainage area. Only
58 gages that meet specific screening criteria (accuracy of reported drainage area, period of record, number
59 of years of record) are used (McCay, et al., 2012).

60 Unmodified, the NHDPlus EROM model provides annual average flow estimates for medium
61 resolution (100 K) hydrographic stream reaches defined by the National Hydrography Dataset. CCDFE
62 uses the EROM annual flow estimates as the basis for more spatially and temporally explicit estimates of
63 flow, adjusted with locally available flow gages and verified with measured stream flows. CCDFE
64 describes flow at CCAMP Coastal Confluence monitoring sites at daily resolution. and reconciles the
65 following issues inherent in the NHDPlus EROM model because of its national scale: (1) CCDFE allows
66 use of flow data from more locally available stream gages that may have a shorter period of record or that
67 may otherwise not be employed in the EROM calculations , (2) CCDFE allows for flow adjustments
68 using gages from nearby watersheds with similar hydrologic, climatic, and land use characteristics , (3)
69 CCDFE makes use of monthly measured flow data at coastal confluence sites to optimize choice of gages
70 and to assess “fit” of the model.

71 Richards (1997) addresses the challenges associated with load estimates developed from
72 recording flow gages paired with infrequent interval analyte grab samples. He offers several methods for
73 addressing these challenges, some of which are employed here. Others have compared the performance
74 of various estimation approaches and generally note that bias increases and precision decreases with
75 sampling interval (Stelzer et al., 2006; Birgand, et al., 2011; Zamyadi et al., 2007). Birgand et al. (2011)
76 reported uncertainties of +/- 40% for monthly sampling of most nutrients using either straight linear
77 interpolation or a ratio approach where annual flow volume is multiplied by annual flow-weighted
78 concentration (generated from monthly measurements). Stelzer et al. (2006) addresses the issue o

79 f “flashiness”, a measure of day-to-day flow variation, where streams that are highly flashy are more
80 influenced by sampling frequency than less flashy flow systems. This can result in higher bias and/or
81 lower precision in modeled load estimates.

82 Studies have shown that for some analytes there is a “diluting” effect with increased flow,
83 whereas with other analytes the opposite is true. Birgand et al. (2011) report a concentrating effect with
84 increased flow for analytes associated with particles (including phosphorus and total suspended solids), a
85 diluting effect for soluble analytes such as dissolved organic carbon, and mixed effects for nitrogen
86 analytes. Stelzer et al. (2006) reported an exponentially declining effect associated with dissolved silica.
87 These effects can result in loads to either be over-estimated or under-estimated by straight linear
88 interpolation (Stelzer et al., 2006; Birgand et al.).

89

90 **Methods**

91 Field Data Collection - Monthly flow and nutrient data are collected by CCAMP in accordance
92 with California State Board’s Surface Water Ambient Monitoring Program Quality Assurance Program
93 Plan (www.waterboards.ca.gov/water_issues/programs/swamp/). Depth-integrated samples are collected
94 into 1 L plastic bottles from the center of the stream flow or thalweg and immediately placed in cold ice
95 chests (4 °C) for transport to the laboratory for nutrient analysis. Flow measurements used for validation
96 of the CCAMP stream flow estimation model are typically collected monthly along a ten-point cross
97 section using a Marsh-McBirney conductive probe flow meter and setting rod. In locations where this is
98 not feasible (for example at culverts) other methods of estimating cross-sectional area are used.

99 Central Coast Daily Flow Estimation (CCDFE) - CCAMP enhancements to the NHDPlus EROM
100 model include selection of one to three USGS gages that more directly represent localized flow conditions
101 at the site of interest. Gages are also selected to ensure that flow data throughout the time period of
102 interest is available from at least one gage at any given time. In some cases a gage may reside on the same
103 stream system as the site of interest. These gages may not be represented in the existing EROM model
104 because of its required period of record and other criteria. Ratios are developed between gaged daily flow

105 measurements and the EROM annual mean flow at each gage location. If more than one gage is used
106 these ratios are averaged. Mean daily flow ratios are then multiplied by the NHDPlus-derived annual
107 mean daily flow at the discharge location of interest to estimate flow at that location and point in time.
108 Gage choice is optimized by evaluating performance against CCAMP measured monthly stream flows,
109 collected since 2005. Measured flows provide benchmark data for flow model validation, through simple
110 linear regression. In some cases, flow has not been collected at the site of interest. In two of these cases,
111 the San Lorenzo and Pajaro rivers, modeled flow was benchmarked against measured flow collected at
112 upstream sites, after adjusting for difference in watershed area.

113 Load Assessment Including Adjustments for Dilution effects - The bulk of the concentration and
114 measured flow data available for the coastal loading assessment is collected at monthly intervals via the
115 CCAMP coastal confluences monitoring program. We initially explored using linear interpolation to
116 impute concentration values for days between two consecutive measured concentrations (Chescheir, et al.,
117 2010; Birgand et al., 2010; Zamyadi et al. 2007). Because of the monthly sampling interval, these
118 estimates are likely to have a relatively high degree of error; Birgand et al. (2011) estimated 30 to 80%.

119 We observed that, depending on the watershed, some analytes display concentrating effects with
120 additional flow, whereas others show diluting effects; this effect has been noted by others in other
121 locations (Chescheir et al., 2010; Birgand et al, 2011; Stetzer, et al.). We also noted that this effect could
122 vary in different watersheds depending on source of pollutant; point sources tended to dilute with flow
123 increases, whereas in some instances non-point sources tended to concentrate. In order to improve our
124 estimates we determined that we should account for these effects where they are statistically significant.

125 We developed an algorithm to scan site-level analyte - flow relationships to identify possible
126 concentrating or dilution effects. The scanning algorithm employs flow interval, ratio estimation, and
127 regression approaches (EPA, 2003; Richards,1997). We created 30 logarithmically scaled bins for
128 characterizing flow ranges. For all sites and analytes of interest, we produced tables of average
129 maximum and minimum concentrations within each of the 30 flow bins. For each site – analyte
130 combination, we used linear regression to calculate coefficients of determination on average

131 concentration and the lower boundary of the respective flow bin. We successively removed low-end flow
132 bin values from the regression, until either the p-value was less than 0.05 or fewer than six flow bins
133 remained. The intent in doing this was to eliminate lower flow relationships with concentrations that may
134 be dominated by factors other than runoff (such as groundwater contributions, local effects, etc.). Only
135 sites with significant positive or negative relationships between flow and concentration were adjusted for
136 diluting or concentrating effects.

137 After we determined which relationships were significant, values were imputed for empty bins
138 using linear interpolation between bin values on either side of the empty bin(s). Values were calculated
139 for both bin maximums and minimums. Appendix A shows analyte relationships for all sites, using
140 nitrate as an example (John – not yet developed...we may or may not want this in the report).

141 For site - analyte combinations where linear regression showed a significant increasing or
142 decreasing slope, adjustments were made to incorporate concentrating and diluting effects. Adjustments
143 were made using a hybrid algorithm involving both flow interval and ratio estimator approaches
144 (described by Richards, 1997 and EPA, 3002). The maximum and minimum concentration/flow ratios
145 were calculated for each flow bin. In the case of diluting effects, the maximum concentration in the bin
146 was divided by the lower flow bin boundary. This provides the most conservative estimate of maximum
147 dilution effect for that flow regime. In the case of concentrating effects, the minimum concentration in
148 the bin was divided by the lower flow bin boundary. This provides the most conservative estimate of
149 minimum concentrating effect for that flow regime.

150 The hybrid algorithm utilizes linear interpolation between two monthly measured concentrations
151 to establish a trial concentration for each day that lacks a measured concentration. Where no significant
152 diluting or concentrating relationship is detected, the trial concentration is used as the imputed
153 concentration. For site - analyte combinations that show significant dilution effects, the maximum daily
154 flux is multiplied by the modeled flow to derive a maximum concentration. When a trial concentration
155 exceeds the calculated maximum concentration, then the maximum concentration is used as the imputed
156 value. If the trial concentration does not exceed the maximum concentration, the trial concentration is

157 used as the imputed value. In the case of site - analyte combinations with significant concentrating
 158 effects, when a trial concentration is less than the calculated minimum concentration, then the minimum
 159 concentration is used as the imputed value. If the trial concentration is not less than the minimum
 160 concentration, the trial concentration is used as the imputed value.

161

162 **Results**

163 Linear correlations between model results and measured stream flows for most coastal confluence
 164 sites are relatively high. R-square values for the twenty-eight benchmarked sites range from 0.307 to
 165 0.988 and average 0.756. Slopes range from 0.877 to 1.663 and average 1.077 (Table 1). Some
 166 watersheds present more modeling challenges, depending on gage location, anthropogenic disturbance,
 167 and watershed behavior. For example, the Santa Maria River is highly influenced by extractions,
 168 irrigation runoff, and by an upstream reservoir. The Old Salinas River has flow influence from the
 169 Salinas River via a tide gate during higher flow events, and is heavily influenced by irrigation runoff and
 170 tile drain water. Field measurements at some sites are confounded by tidal influence and/or access
 171 problems. The coastal confluence sites which are not routinely measured for flow by CCAMP crews
 172 include Scott Creek (tidal influence), San Lorenzo River (not wadable), Pajaro River (not wadable), Old
 173 Salinas River and Tembladero Slough (tidal influence), Little Sur River (no access), and Mission Creek
 174 (limited access). Of these, Pajaro and San Lorenzo rivers were benchmarked using upstream site data,
 175 and Mission Creek was benchmarked using a relatively limited dataset.

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SiteTag	Waterbody	R-squared	Slope
304APW	Aptos Creek	0.8815	1.0008
304GAZ	Gazos Creek	0.9692	0.9890
304LOR	San Lorenzo River*	0.9596	0.9898
304SOK	Soquel Creek*	0.9392	1.0102
304WAD	Waddell Creek	0.7543	1.0631
305THU	Pajaro River*	0.9879	0.9979
307CML	Carmel River*	0.9555	1.0842
308BGC	Big Creek	0.7586	0.9895
308BSR	Big Sur River*	0.9712	1.0883

308WLO	Willow Creek	0.6703	1.0419
309DAV	Salinas River*	0.9667	1.0309
310ADC	Arroyo de la Cruz	0.5681	1.0532
310ARG	Arroyo Grande Creek*	0.5278	0.9972
310PIS	Pismo Creek	0.7040	1.0045
310SLB	San Luis Obispo Creek	0.8163	1.0114
310SRO	Santa Rosa Creek	0.8590	0.9987
310SSC	San Simeon Creek	0.9014	1.1805
310TWB	Chorro Creek	0.5932	0.8765
312SMA	Santa Maria River*	0.3963	1.4918
313SAC	San Antonio Creek	0.7309	0.9965
314SYN	Santa Ynez River*	0.6485	1.0792
315ABU	Arroyo Burro	0.9317	1.1794
315ATA	Atascadero Creek (S Barbara Co.)		
315CRP	Carpinteria Creek	0.3272	1.1748
315FRC	Franklin Creek	0.3068	1.0643
315GAV	Gaviota Creek	0.8636	1.6632
315JAL	Jalama Creek	0.5773	1.0009
315RIN	Rincon Creek	0.8565	1.0281

177 Table 1. R-square values and slopes of regressions relationships for benchmarked coastal confluences. *

178 denotes at least one of the gages is present in the watershed being modeled.

179

180 Notes for future analysis – We need to look at how the loading values differ between this
 181 approach and a straight linear interpolation. It would be good to be able to say, % difference in
 182 total loading varied from x% to y% in estimates that were adjusted based on a significant diluting
 183 or concentrating

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185 We should develop a Table of site – analytes with significant relationships and note direction of
 186 change.

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255 Appendix A. Flow – analyte relationships, using Nitrate + Nitrite as an example. Graphs in column A
256 show all concentration and flow data used in the analysis. Graphs in column B show average
257 concentrations in each flow bin, and the associated regression lines. The longer line is for the
258 entire set of flow bins; the shorter red line is for higher end flow bins where R-2 exceeds 0.5.
259 Graphs in column C show bin values after a smoothly algorithm is employed and missing values
260 are imputed. Relationship for other analytes can be found at

Methods for Estimating Pollutant Loads (Richards, 1997)

Numeric Integration — Total load is calculated as the sum of the individual loads calculated for each sample.

Worked Record Procedure — Chemical observations are plotted onto a detailed hydrograph, and smooth curves are drawn through chemical data points based upon analyst's experience with the relationship of concentration and flow.

Averaging Approaches — Calculation that uses averaging of concentration and/or flow to estimate loads. For example, analyst might multiply average weekly suspended solids concentration by daily flow to estimate daily loads for the week.

Flow Interval Technique — Semi-graphical technique that calculates "interval loads" as the product of average flux for a range of daily flow values times the number of days in which flows were within the particular flow range.

Ratio Estimators — Total loads are estimated using a known relationship between the less-frequently sampled parameter of interest and a more-frequently sampled parameter (e.g., discharge) to fill gaps in the data record for the parameter of interest.

Regression Approaches — Relationship is established between concentration and flow based on samples taken, and then applied to estimate concentration for days not sampled.

Flow-Proportional Sampling — Mechanical approach in which representative samples are taken to determine concentration for a known discharge. Pollutant load is calculated as the sum of the sample concentrations multiplied by the measured discharge.

262

263 Figure From usepa 2003

264

265 Notes below:

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267 Estimating Loads with available data

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269 Given constraints of the available dataset:

270 Analyte concentrations were measured monthly

271 Flows were measured monthly when conditions permitted such measurements

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273 We pursued an approach guided by tenets set forth in Richards,1997

274 "

275 1. Find a way to estimate "missing" concentrations: i.e. concentrations to go with the flows observed at
276 times when chemical samples were not taken.

277 2. Abandon most of the flow data and calculate the load using the concentration data and just those
278 flows which were observed at the same time the samples were taken.

279 3. Do something in between - find some way to use the more detailed knowledge of flow to adjust the
280 load estimated from matched pairs of concentration and flow.

281 The second approach is usually totally unsatisfactory because the frequency of chemical observations is
282 inadequate to lead to a reliable load estimate when simple summation is used. Thus almost all of the
283 load estimation approaches which have been shown to give good results are variants of approaches 1 or

284 3. Total load vs. unit load

285 If all of the flow and concentration observations are available for all n intervals in formula (3) or (4)
286 above,

287 the summation is an easy task. The summation is the total load for the time period of interest; each
288 individual product, $c_i q_i \Delta t$ or $c_i q_i t_i$, could be called the unit load. If the total load is an annual load, the
289 unit

290 load might be the daily load. If the total load is a weekly load, the unit load might be the hourly load.

291 This distinction is important, because we tend to focus on the total load as our goal. The considerable
292 complexities of the various methods for calculating loads, however, are almost always related to trying to
293 accurately characterize the unit loads. Once this is done, the total load is easily obtained.

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296 We addressed flow measurement issues through use of the ccamp flow model (Worcester, Paradies,
297 initially presented at the 6th National Water Quality Monitoring Conference, Atlantic City NJ 2008)

298 Daily flows were estimated using the ccamp flow model

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300 We addressed issues associated with flow dependent concentration variability in the following fashion:

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302 We initially explored using linear interpolation to impute concentration values for days between measured

303 concentrations.(as in Chescheir etal and other studies)

304 Exploratory data analysis revealed that site specific relationships existed between concentrations and

305 flows. (as in Birgand etal, Stelzer etal,Zamyadi etal and other studies)

306 In some instances concentrations were reduced as flows increased.(as in Birgand etal, Stelzer

307 etal,Zamyadi etal and other studies)

308 In some instances concentrations were increased as flows increased.(as in Birgand etal, Stelzer

309 etal,Zamyadi etal and other studies)

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311 We were concerned about the subjectivity associated with graphical identification of concentration and

312 dilution effects (e.g. the K. Worcester pers comm and the USGS 'worked record' methodology).

313 We explored various methods of detecting the presence of these relationships.(we found no literature

314 which provided an automated scanning methodology for detecting possible concentration or dilution

315 effects)

316 We adopted a hydrid approach for scanning site - analyte combinations to identify possible concentration

317 or dilution effects.

318 The scanning algorithm employs flow interval, ratio estimation, and regression (as described in EPA 841-

319 B-03-004, July 2003 and Richards,1997).

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321 We calculated average concentrations at each site in each of 30 flow interval-regime bins to produce a

322 table of of limits for each flow interval regime

323 We successively calculated the regression based coefficient of determination (R squared) for average

324 concentration in each flow regime for each site analyte combination

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in stepwise fashion beginning with all flow regimes and successively eliminating low flow regime values one bin at a time until an R squared value exceeds .5 (or not)

The slope of the regression line is used to distinguish between concentration and dilution effects.

Notes:

The use of regression here is used only to detect site-analyte situations where concentration - dilution adjustments are needed.

The results of the regression are not used in the process of 'load estimation'.

We explored various methods of improving load estimates which address detected site specific relationships.

We adopted a hybrid approach based on a framework set forth in EPA 841-B-03-004, July 2003 and Richards, P 1997.

The hybrid approach includes:

A 'worked record' approach (as described in EPA 841-B-03-004, July 2003 and Richards, P 1997) modified to utilize the flow regime algorithm described above to mitigate the subjectivity normally associated with the 'worked record' approach with respect to dilution and concentration effects.

A 'flow interval' approach (as described in EPA 841-B-03-004, July 2003 and Richards, P 1997) which utilizes the flow interval regimes described above to impute daily flux, but not to calculate loads for more than a single day.

A 'ratio estimator' approach (as described in EPA 841-B-03-004, July 2003 and Richards, P 1997) which utilizes the flow interval regimes described above to impute daily flux, but not to calculate loads for more than a single day.

351 The hybrid algorithm initially utilizes linear interpolation to establish a trial value for concentration for
352 each day which is missing a concentration measurement.

353 In the case of dilution effects; When a trial value exceeds the average concentration in a given flow
354 regime, the average concentration for the flow regime is used as the imputed value.

355 In the case of concentration effects; When a trial value is less than the average concentration in a given
356 flow regime, the average concentration for the flow regime is used as the imputed value.

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358 Error associated with linear interpolation was examined in more detail using high frequency
359 nitrate concentration data from an in-situ ultraviolet spectrophotometer sensor, deployed by
360 Monterey Bay Aquarium Research Institute through its Land Ocean Biogeochemical Observatory
361 (LOBO) network. The L03 sensor is located at the lower end of the Old Salinas River in Moss
362 Landing Harbor. This instrument collects nitrate readings continuously at an hourly interval and
363 has been in operation since 1994. Its location in a tidal area presents additional sources of
364 variability that would not be encountered were the sensor located in a non-tidal riverine
365 environment. We adapted this data for use by selecting daily measurements collected at salinity
366 low points. We extracted monthly interval measurements from this dataset and used the subset to
367 create a daily linear interpolation of nitrate concentrations. Linear regression between the
368 measured and interpolated daily concentrations produced a significant relationship ($y = 0.7228x$
369 $+4.7881$; $P=0.00$, $r^2 = 0.53$). When averaged daily interpolated concentrations were compared to
370 averaged measured concentrations for the period of record, the interpolated values underestimated
371 average concentrations by 3%.

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